STANDARDS FOR ELECTRICAL MACHINES & TRANSFORMERS

GERMAN, BRITISH & AMERICAN STANDARDS COMPARED

BY

FRIEDRICH NETTEL



SPRINGER-VERLAG BERLIN HEIDELBERG GMBH 1923

COMPARISON OF PRINCIPAL POINTS OF STANDARDS FOR ELECTRICAL MACHINERY

(ROTATING MACHINES AND TRANSFORMERS)

BY

DIPL.-ING. FRIEDRICH NETTEL CHARLOTTENBURG

Standards compared:

GERMANY:

Verband Deutscher Elektrotechniker (VDE)

a) Regeln für die Bewertung und Prüfung von elektrischen Maschinen. R. E. M. 1923 b) Regeln für die Bewertung und Prüfung

von Transformatoren. R. E. T. 1923

BRITAIN:

- 1. British Engineering Standards Committee. (B. E. S. A.):
- a) Standardization Rules for Electrical Machinery No. 72-1917.
- b) British Standard Specification for the Electrical Performance of Industrial Motors and Generators with Class A Insulation.

 No. 168 1923.
- 2. British Electrical and Allied Manufactures
 Association. (B. E. A. M. A.):

Standardization Rules for Electrical Machinery. Fourth Edition 1920. Provisionally adopted.

U. S. A.

Standards of the American Institute of Electrical Engineers (AIEE) 1922 Revision

(Excluding Railway- and Tramway Motors and non-stationary Railway Transformers.)



ALL RIGHTS RESERVED

ISBN 978-3-662-24405-0 ISBN 978-3-662-26529-1 (eBook) DOI 10.1007/978-3-662-26529-1

Copyright 1923 by Springer-Verlag Berlin Heidelberg Originally published by Julius Springer in Berlin in 1923.

Preface.

The necessity and importance of the standardization of electrical apparatus was recognized in Germany as early as 1894 and the first rules ("Sicherheitsvorschriften für elektrische Starkstromanlagen gegen Feuersgefahr") came into force in that country in 1895.

In the U. S. of America the first discussion on Standardization of Generators, Motors and Transformers took place in 1898 which resulted in the appointment of a Committee and the subsequent acceptance of the rules proposed by it.

In England the British Engineering Standards Association was formed in 1901. In connection with the British Standards an explanatory note appears necessary: The B.E.S.A.'s rules have for many years been the only generally accepted Standards. Since 1913 the British Electrical and Allied Manufacturers Association, representing the most important powerful British manufacturing firms, have issued Standardization Rules of their own which have attained considerable commercial importance. A special edition of these rules has been issued for export work which on the whole are guided by ideas similar to those embodied in the B.E.S.A. rules. As far as can be gleaned from the article in the "Electrical Review" (Vol. 86 Nr. 2, 216, April 16th 1920) it is intended to publish a new revision of the B.E.S.A.'s rules which will probably contain some of the recommendations of the B.E.A.M.A., so that this will probably mean the return to one single system of Standards for Britain.

The B.E.A.M.A.'s rules being provisional and less important than the B.E.S.A.'s rules are treated in separate Appendices.

In this connection the International Electrotechnical Commission Rules must also be mentioned which were adopted at the Plenary Meeting held in London 1919. It must be hoped that some day an international agreement on the most important points of Standardization of Electrical Machinery will be arrived at.

The I.E.C. Rules have not been included in the comparison because in practice they do not form yet the basis for important contract specifications for which as a rule one or the other national system of standards is still preferred. These rules are also very similar to the A.I.E.E. rules except in less important details.

In December 1922 a meeting of the I.E.C.'s Advisory Committee took place in Geneva. The main topic was the question of rating. After considerable discussion, a proposal on the lines desired by the Preface.

British delegates was agreed to for submission to the National Committees to the effect that overload ratings within the I.E.C. maximum continuous rating be recognised and that, for general industrial machines (the class to be defined later) where overloads have to be provided, the overload only to be applied under such conditions of air temperature as will not cause the limits of maximum temperature laid down by the I.E.C. to be exceeded, viz. 50°C for Class A Insulation measured by thermometer at a maximum ambient air temperature of 40°C.

This means clearly that the overload can only be applied at ambient air temperatures below 40°C.

As far as Britain is concerned Report No. 168—1923 of the B.E. S. A. contains the Standard specification for Industrial Motors and Generators i. e. Machines from I B.H-P. or kVA upwards with Class A Insulation wound for voltages not exceeding 7000 Volts having both Continuous- and Short-Time Ratings. — This report came to hand only late but it was possible to include the principal requirements which are marked thus:) <

In this connection it is important to note that the American delegates have declared that they object to the Geneva proposals. Under these circumstances an international agreement on this important question does not appear to be within easy reach.

In the various countries quite a number of revisions appeared necessary which had to take into consideration not only the enormous strides made by the different branches of Electrical Engineering, but also the experience gained in the application of the rules.

The study of the latest editions of the Standards of the three countries mentioned above, (the inclusion of other countries would not have been conducive to lucidity), shows that the views adopted on the principal points are related closely enough to allow a proper comparison to be made.

The purpose of this booklet is to enable the engineer or merchant buying from or selling to foreign countries, to inform himself *quickly* on any of the principal points telling in the design and performance of electrical machinery which he may be called upon to judge.

It is hoped, however, that it will also be of some use to the student and even to the consulting engineer in framing specifications.

For manufacturers and in cases of disputes, where legal decisions are involved, it will always be necessary to fall back on the original wording of the rules published by the bodies mentioned on the frontispiece; even in cases like this, the collation with the practice adopted in another country may afford guidance for the settlement of disputed points, on which the rules of the respective country might not prove precise enough.

Contents.

Section I.

Rotating Machines, excluding Railway- and Iramway-Motors
Standard pressures and Frequencies
Rating-Classification
Heating
a) Standard- and max. permissible Temperatures of cooling media
b) Determination of End Temperatures and Temperature Rises. Heating
Test
c) Method of measurement of Temperature of the cooling media 10
d) Method of measurement of Temperature Rises
e) Correction of Temperature Rises for Altitude
f) Permissible Temperature Rises
High-Pressure Tests and Insulation Resistance
1. High-Pressure Test
2. Surge Test (Germany only)
3. Winding Test and Insulation Resistance Test
Efficiency
I. General
2. Determination of Losses for Conventional Efficiency Test 2:
Inherent Regulation
Overspeed Test
Tolerances
Appendix to Section I.
British Electrical and Allied Manufacturers' Association Rules (B.E.A.M.A
Rules)
Section II.
Transformers.
Rating-Classification
•
Heating
b) Determination of End-Temperatures and Temperature Rises 3
c) Methods of measurement of Temperature of cooling media 3
d) Methods of measurement of Temperature Rises
e) Correction of Temperature Rises for Altitude
f) Permissible Temperature Rises

6 Contents.

pag	
High-Pressure Test and Insulation Resistance	Ş
1. High-Pressure Test	
2. Surge Test (Germany only))
3. Winding Test and Insulating Resistance Test)
Working in parallel (Germany only))
Overloads)
Efficiency, Transformer Losses	ĺ
I. General	Ĺ
2. Classification of Losses and their measurement	1
Inherent Regulation	Ĺ
Tolerances	1
Appendix to Section II.	
British Electrical and Allied Manufacturers' Association Rules (B.E.A.M.ARules)	2

SECTION I. Rotating Machines.

Standard pressures and Frequencies and Classification of Rating.

Ger	many		Britain		U. S. A.
Generators	Motors	Motors	Consumer	Station	
1. D. C. (Generators a	nd Motor	s. Volts.		The second of th
115	IIO	110		idustrial ines (
230	220	220	220	242	
460	440	440	440	484	none
		460			
		500			
2. Three-	phase A. C.	Generato			olts.
130	125			ndustrial ines (
230	220	220	240	264	
400	380	400	416	457	
525	500	500			
3150 3000			3000	3 300	none
5250 5000			6000	6600	
6300	6000		(10000)	(11000)	
10500	10000				
15750	15000				
3. Freque	ncies. Cycl	es per se	cond.		
	50		50		60 (usual)

8 Section I.

Rating-Classification.

Germany	Britain	U. S. A.
a) Continuous Rating. The machine shall give its rated output for any desired period without exceeding the limits specified for observable temperature and temperature rise.) a) The British Standard for Continuous Rating is the output at which a machine can work for an unlimited period and comply with these rules.	a) Continuous Rating. A machine rated for cont. service shall be able to operate continuously at its rated output without exceeding any of the rules.
b) Short-time Rating. The machine shall give its rated output for the specified period without etc. (as above).	b) Standards for Short-time Rating. 1. One hour Rating. The output at which a machine can work for one hour and comply with the rules. 2. One half-hour Rating. The output at which a machine can work for one half-hour and comply with the rules. (b) Short-time Rating. A machine rated for short-time service shall be able to operate at its rated load for the time specified in each case without exceeding etc. (as above). Standard Short-time ratings: 5, 10, 15, 30, 60, 120 minutes.
c) Duty-cycle Rating. Periods under pressure are followed by periods during which the machine is switched off the total duration of the cycle being max. 10 minutes. The intermittency viz. the ratio of the period during which the machine is under current to the duration of the cycle characterizes the duty-cycle. The machine shall be able to work on a uniform duty-cycle service without the specified temp. limits being exceeded. Standard values for intermittency: 15, 20, 40%.		c) Duty-Cycle Rating. For purposes of rating either a continuous or a short-time equivalent load may be selected, which shall simulate as nearly as possible the thermal conditions of the actual duty-cycle. d) Nominal Rating. For Railway substation machines see as for transformers page 32.

Heating.

Germany	Britain	U. S. A.
a) Standard- and max.	permissible Tempera	atures of cooling Media.
Normal: 20°C	none specified	25°C (water)
*) Highest permissible: 35° C	40 °C (air)	40°C (air)
•	> 30 ° C (air) **) ⟨	
*) on this Temperature th	e End Temperatures	on page 12 are based.
		ied on page 19 is required.
1		the finds of the first milk
b) Determination of I	End Temperatures as Heating Test.	nd Temperature Rises.
The heating test is to be	The temperature	Whatever method of tem-
carried out at rated load	l -	perature measurement (see
	out at rated output	Section d) be employed
		it is required that:
1) for machines with con-) 1) for machines with	i) The temperature test
tinuous rating until the tem-	continuous rating until	of a machine for continuous
perature does not rise no-	sufficient evidence is	service shall be continued
ticeably but not longer than	available to show	until sufficient evidence is
10 hours.	that the max. tempe-	available to show that the
	rature and temp, rise	maximum temperature and
	would not exceed the	temperature-rise would not
	requirements of the	exceed the requirements
	rules if the test were	of the rules, should the test
·	prolonged until a	be prolonged until the at-
	steady final tempera-	tainment of a steady final
1	ture were reached.	temperature.
2) for machines with short-	2) for machines with	2) The duration of test
time rating for the specified	short-time rating for	of a machine with a short-
time, the testing being	the time required by	time rating shall be the time
started with machine cold	the rating. (required by the rating. It
or when the Temperature		shall commence only when
of any part of the winding		the windings and other
is not higher than 3 °C than		parts of the machine are
the Temperature of the		within 5°C of the ambient
cooling medium.		Temperature.
3) for machines for duty-	17-4-0 T1 - 4	37.4
cyclerating until the tempera-	Note: The tempe-	Note: A machine may
ture does not rise noticeably.	rature test shall be	be tested at any convenient
The temperature is con-	carried at any con-	ambient temperature pre-
sidered constant if the rate	venient air tempera-	ferably not below 10°C.
of increase does not exceed	ture not exceeding	

40 ° C.

20 C per hour.

Continuation: Heating.

Germany Britain U. S. A.

c) Methods of measurement of Temperature of the cooling media.

Same as Britain but | > The air temperature shall "cooling media".

With large machines having parts beis admissible for test equal to the temperature outside of the pit.

For machines with current of incoming air. (forced draught-andwater-cooling see Transformers Note page 34.

generally valid for be taken as the mean of the readings of the thermometers taken at equal intervals of time during the last low the floor-line it quarter of the duration of the test. - For a pipe venpurposes to make tilated or forced draught the pit-temperature machine, the air temperature is to be measured by a thermometer placed in the

Same as Britain but for Forced draught machines a weighted mean shall be employed, a weight of four being given to the temp. of the circulating air and a weight of one to the room air. -Where machines are partly below the floor line the temp. of the rotor shall be referred to a weighted mean of the pitand room temp. relative to the rotor portions in and above the pit. Stator parts in the pit shall be referred to the temp. in the pit.

d) Methods of measurement of Temperature rises.

The Temperature of windings is defined as the higher of the two values as below:

- 1. Mean Temperature rise by the Resistance Method.
- 2. Temperature rise of the hottest accessible spot measured by Thermometer (mercury or alcohol). Where Resistance Method is not applicable the Thermometer Method shall be used alone.
-) 1. Thermometer Method. Several thermometers (mercury or alcohol) shall be applied to the hottest accessible stationary parts during the test period and other thermometers to the rotating parts as soon as the machine is stopped †). (

2. Resistance Method.

- The temperature rise shall be calculated from the resistances hot and cold, and the initial temperature (by thermometer) of the winding itself. Thermometer measurements shall also be made to ascertain if there is any higher observable temperature. If such is found it shall be adopted as the maximum observable temperature.
- 1. Thermometer Method. Mercury, alcohol, resistance or thermocouple thermometers applied to the hottest accessible part of the completed machine.

2. Resistance Method.

Consists in the measurement of the temperature rise of windings by their increase of resistance. In the application of this method thermometer measurements shall also be made whenever practicable without mantling the machine. The higher temperature of the two shall be taken as "observable" temperature.

Continuation: Heating.

d) Methods of measurement of Temperature rises.

Germany	Britain	U. S. A.
(Temp. Coefficient of copper = 235.)	3. Embedded Temperature Detector Method same as U. S. A. but when specified with the enquiry only ††). Compliance with Methods I & 2 is however decisive. (Temp. Coeffic. of copper = 234,5.) Special cases: D. C. Motors and Generators. Field coils Method 2 or Method I and 5°C lower Temp. rise. Synchronous Motors and Generators. Field windings: Method 2. Stator: Method 2 or Method I and with 5°C lower temp. rise*). Induction Motor or Generator. Stator & Rotor Method 2 or Method I with 5°C lower temp. rise*). *) For Machines under 5000 Volts Method I with 5°C lower temp. rise*). *) For Machines under 5000 Volts Method I alone is also permissible. Note: †) > For industrial machines thermometer Method is used only. (††) Method 3 shall be employed for machines over 3000 kW for rated pressures exceeding 3300 Volts	3. Embedded Temperature Detector Method consists in the measurement of the temperature rise by thermocouple or by resistance temperature detectors, located as nearly as possible at the estimated hottest spot. When required to be checked by method 2. (Temp. Coefficient of copper = 234,5.) Note: Method 2 shall not be used for circuits of low resistance (other than transformer windings) as interpole windings. Method 3 should be applied to all Stators of machines having a width of 50 cm or over. It should also be applied to all machines of 5000 Volts or more, if rated over 500 kVA regardless of core width.
e)	Correction of Temperature Rise	es for Altitude.
The rules hold good for service at altitudes up to 1000 m over sea level. If a machine will have to work in high altitudes this must be specially stated.	vice at an altitude over 1000 m (3300 ft.) the observable temperature rise if tested near sea level shall be reduced 2 ¹ / ₂ per cent for each 1000 feet. > For industrial machines as above but reduction 1 ¹ / ₂ , ner cent	Generally the height above sea level at which a machine is intended for work is assumed not to exceed 1000 m. It is recommended that when a machine is intended to work at altitudes above 1000 m the permissible temperature rise at sea level shall be reduced by 1 per cent for each 100 m by which the altitude exceeds 1000 m.

f) Permissible Temperature Rises (ET = End Temperature; TR = Temp. Rise).

12

	Ge	Germany					מַ	britain				U. S. A.	į		
					For		essures up to	5000 > 7000 (Volts *)	\ \ \	lts *)			Open Types**)	ypes *	*
Item	Class of Insulation	Part of machine	ET °C	TR °C	Line	Мегрод	Class of Insulation	Part of machine	ET °C	TR °C	Method measure	Class of Insulation	Part of machine	ET °C	TR
	7 200 7	A.C. Stator windings in slots	7.5	40	н		Class D	A.C. windings in slots	85	45	H	;		75	35
1	cotton Not silk simpreg-	All other windings			10		same as class I	Rot. armatures with commutat.	80	40		Class O same as Germany Class I	sgui v	0	•
79	paper) nated	except Item 9 & 10	85	20	3			Stat. and rotat. D.C. field coils	85	45	N .		bniw b voled b	8	5
	Class II:	1,7,0	,		4	·	Class A	as line I	95	55	-	Class A	ləil ətate	5	٤
8	cotton imprag-	as Item 1	3	5	'n		Germany	as line 2	8	20	-	same as Germany class II also when	gs s gs	3	2
	silk (not oil- paper jimmers.)	as Item 2	95	9	9	əpuı	ciass II also oil-immers.	as line 3	95	55	7	oil-immersed	sl-əl; aiba	95	55
	Class III:	All windings				1 53	~	not tot. enclosed) 40 (gnia iw		
- V	ac ac		95	9	6 a	ısı	Industrial	tot. enclosed	pasc	> 20 <			nn ted		<u>-</u>
	paper pound	Items 9 & 10				Ren		short time rated		>20 <			th: inor		
9	Class IV:	as Item 5	95	9	~ ∞	əəs	Enamelled	as line 1	95	55 50	1	Class A	other ort ci	8	50
·	Enamelled Wire				6			as line 3	95	55	69	Luamenca wire	ap S.a	95	55
	Class V:				ខ		Class B	as line 1	115	7.5	•	Class B	niba bas	9	10
	Mica, Aspestos pre- parates if binding matter may be de-	as Item 5	115	8	I	- •	Mica, Asbes- tos and simi-	as line 2	110	70	-	same as Germany	!M	2	2
	stroyed without im-				12		lar material	as line 3	115	7.5	6	class V		115	75
	Class VI:		Restricted	icted flu-			Class C, fire		no limits	mits		Class C		no limits	nits
∞	Naw Mica, Porcelain, fire proof materials	as Item 5	ence on adjacent parts only	on cent only	13		refractory material	I	yet spe-	et spe-	I	same as Germany class VI	ET TR	yet spe- cified	pe- ed

6	Classes I-VI	Single-layer field coils with expo- sed surfaces	100 65	-					Part of machine single-layer field coils (on stator and rotor) with expo-	Clas	Insulation S Q) Class B
10	Classes I-VI	Continu- ously short	5°C higher than Items 1-7	14	-	insulated	100 Restri	11 1	sed Other	(80) (40) (80) (40) 95 55	120 80
=	uninsulated	windings	as Item 8	15		uninsulated	windings ence on adjacent parts only	l l	Rotor windings	₩ <u> </u>	110 70
12	ı	Iron core without embedded windings	as Item 8	91	н		Iron core without sa line embedded 15 \langle windings	1 11	in slots Short circ. wind-	(80) (40) 95 55 (85) (45)	
13	ı	Iron core with embedded windings	as Items I-7	17	-	1	Iron cores as lines with I—12 embedded \(\) windings \(\)		ings insulated on stat, and rotat. Cores and uninsul. short circ windings	as B	120 80 n line 15
14	[Commu- tator and sliprings	95 60	81	-		Commu- tators and 90 \	50 1	Commutators, collector rings, bare metallic surfaces	ET IIS	TR 75
15	l	Bearings	80 45		Меthod	Placing of temperature detector	Insulation Class A Class B ET TR ET TR	B	Placing of temperature detector	$ \begin{array}{c c} & \text{Insulation} \\ (Class \ O) & Clas \\ Class \ A & \end{array} $	
91	1	All other parts	as Item 8	61		Between 2 coil-sides in one slot	5°C more than lines 4—6 lines 10—12	-12 3		ET (85)	ET TR 120 80
N _o	No temperature detectors specified.	ectors specif	ied.	20	. s	Between coil- side and core below 5000 Volts Same as line 20 but ow 5000 Volts	approx. same as lines 4-6 10-12 1 ° C more for each 1000 Volts over 5000 Volts than lines 4-6	9 es 3	sides and octa- coil-sides and core For windings with coil-side per slot and detectors be- tween coil-side and core and coil-side and wedge		00 00 00 00 00 00 00 0
Item "	Note. Method of measurement: Items 1—9. Method I. Checked " 10—16. " 2. —	measurement: od 1. Checked 2. —	it: ed by 2	*) Mc 1 ¹ / ₂ ⁰ C J of by v 5000 V. Data industri	h) Mot 20 C 16 by w 50 V. Data kVA	*) Motors and generators over 11/3°C less for each 1000 V or p of by which the rated pressur 5000 V. Data marked thus \ \langle referindustrial machines from 1 B. or kVA upwards, see Preface.	er 5000 art the e excee (also) H.P. k) Wh bare libe *) Fe ii be all v	ers are applance of an area of an area of an area of an area of a shifter than the pt short cir.	ied direct imp. Rise method 1. emp. Rise he values cuited in-

Section I.

1. High-Pressure Tests.

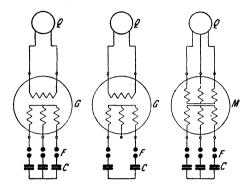
		, ,)	1)	1	1 43 1		ı	1		
	Strength ince	: Strength		frequency; commended	e	rature	Test p	Volts min./max.	006	2 E + 1000	2,73 E'+1000 F' rollage	
U.S.A.	1. Test of Dielectric Strength 2. Insulation Resistance	1. Test of Dielectric Strength	sinusoidal	not less than rated frequency; 60 cycles per sec. recommended	one minute	working Temperature		ĕ	660 Watts or s 0,5 H.P. vol- s tage under 275 V. to 25 V.	all Machines except as otherwise specified (see below)	more than	permanently grounded single phase systems. (Not 3-phase with neutral grounded)
	1. Te 2. Ins	1. 7		not le 60 cyc		F	Winding	Small machi	Small Generators and Motors under	all Mac as other (see	A.C. ma- chines con- nected to	permanel single pl (Not 3-pha gre
	so) to ace.			n 25			Test pressure	min./max. Volts	1	>2000 (above 3 H. P.	1	1
	est tance* efer (als ee Pref	Test		betwee er sec.		ature	Test p	Volts	2 E + 500) 2 E + 1000 (1,5 E +375	1,5E +750
Britain	1. High-Pressure Test 2. Insulation Resistance* Data marked thus \ \ refer (also) to industrial machines; see Preface.	1. High-Pressure Test	sinusoidal	general any between 25 and 100 per sec.	one minute	working Temperature	Rated	Output	below 746 Watts or I H.P.	of 746 Watts or I H.P. and over	below 746 Watts	of and over 746 Watts
	1. Hig 2. Ins Data mark industrial	1. F		rated in		wor	Part of	Machine	all Machines	all Machines	all Machi- nes in ser-	vice (i. e. not new)
	it ndings			. sec.		ure	Test pressure	min. Volts	2 E + 500	2 E + 1000		1
	ure Tes for wii V. urns*	est	oidal	cycles 1	one minute	emperat	1	Volts	3 E	3 E	2 E	+ 5000
Germany	 High-Pressure Test Surge-Test for windings over 2500 V. Test on Turns* 	ligh-Pressure Test	sinusoidal	rated, or 50 cycles p. sec.	one n	working Temperature	Rated Output	terminal pressure E	Output smaller than 500 Watts	Output larger than 500 W. E up to 5000V.	E over	5000 V.
) ~ ~	1. High	Wave form.	Frequency	Duration	Temperature during Test		Winding	j−ə sw	esti tqeo:	cə sZuip	niw IIs
			Wa	Fre	Dai	Ten	u	Iter	æ	م		ပ

min. 1500 max.	3500	min. 1500 max. 3500	l	5000 8000 for for Exciter Exciter Scriter Volts Volts 275 to 750	E+1000	4 E + 1000	0.0_0^{-1} higher than above	I 5 0/0 lower than lowest individual test pressure	of the circuit to which tion Motors the normal
10 E		10 E	5000	5000 for Exciter Volts less than	2 E +	4 E +	20 0/0 than	I \$ 0/0 lo lowest in test pr	circuit otors the
l		for starting with A.C. with field shorts circuited	for starting with A.C. with fields open circuited and sectionalized while starting	for starting with A.C. with fields open circuited and connected all in series while starting	ordinary	reversing	Standard machines produced in large quantities 2500 V.	Assembled apparatus tested as electrical unit	presents: voltage connected. of Induct
in- of ne-					pa d	tors	qua	8 50 50 50 50 50 50 50 50 50 50 50 50 50	E r orm; e is otor
 Field windings of A.C. Gene-	rators	us Machines nverters	of Synchrono	Field windings I gaibuloai	Phase-wound Rotors of In-	duction Motors	Standard in large	Assemble	Note. E represents: The normal voltage the machine is connected For Rotors of Induinduced voltage.
min. 1500 > 2000 (max. 3500	same as field windings	min. 1500 >2000 (max. 3500	1	8000 for Exciter Volts 250,2754 and above	-		1 3	d on the reached ne frame,	machine sure limi-
 王 01	same a	10 E	5000	5000 for Exciter Volts 1ess than 250 >275 <	+ 500 F	+1000 (+ 1000 + 1000 -	be base pressure ig and th	or for a re, press otherwise fore 1.
Separately excited rotating field windings > Exciter volts not over 750 <	Exciter	for starting with A.C. with fields closed- circuited	for starting with A.C. with break-up switch	for starting with A.C. without break-up switch and fields open	non-reversing according to	output as above	reversing	a) Inc test pressure stall be based on the rated pressure or the highest pressure reached between any part of the winding and the frame, which ever is greater, N. For a mochine driven by water-wheal and	exposed to runaway conditions or for a machine exposed to possible excess pressure, pressure limiting devices should be employed otherwise test as under a) is necessary. *) Sequence: advisable a before 1.
Separate rotating fi	Ex	esmines er	of Synchronor	Field windings or Ro	punoM	Rotors of Induction	Motors revers	a) The tes rated pressure between any p which ever is g	exposed to runaway of exposed to possible exting devices should be under a) is necessary. *) Sequence: advise
2 E + 1000	-	2000	2000	nachine	of one	against f asyn-	nanently	j	
3 E		10 E + 1000						e rotor _l pole, per	
with Exciter circuit always closed with or without start-	ing from A.C.	with Exciter winding sectionalized without or with starting from A.C. side	with discon- nectable ex- citer circuit without start- ing from A.C.	as Item f but with starting from A. C. side	E represents:		chines the highest possible pressure against hen one pole is grounded. phase-wound Rotor windings of asyn-	chromous motors; non-reversing; the rotor pressure, reversing; 1,5 times rotor pressure. 4. For machines with one rotor pole, permanently grounded it, times rated pressure. grounded it times rated pressure. Grounded and windings mand not he sered	T Cs
суко-	nys 1	Converter and	ys of Rotary nous Mo	Exciter-windi	Note. E represents	field windi	or more machines the hi the frame when one pol 3. For phase-woun	chronous motors; non-i reversing: 1,5 times roto 4. For machines wit grounded 1,1 times rated	*) Sequence
7		e e	4	90		with	the	reve	

Section I.

2. Surge Test (Germany only).

The surge test which serves to ensure the efficiency of the insulation against surges occurring under ordinary working conditions shall be



made with the completely assembled machine on the factory test bed as far as possible in accordance with the diagrams of connections as shown below for Synchronous- and Asynchronous machines. (G = Generator, M = Motor.)

The machine on test shall be connected to cables or static condensers (C)

over sphere spark-gaps (F) with solid spheres of at least 50 mm diameter.

The Test Capacitance of the cables or condensers shall be as follows:

Rated voltage E kV	Capacitance in each phase min. μF. (Mikrofarads)
2,5 to 6	0,05
up to 15	0,02
over 15	0,01

Each spark-gap shall be set for 1,1 times rated Voltage. The machine shall be excited by a d. c. supply to abt. 1,3 times rated voltage at rated speed or with 3-phase a.c. at rated frequency respectively. The spark-gaps shall be caused to break down in any manner (say by temporarily reducing or bridging of the gap) and the arcing maintained for a period of 10 secs. During the test the spark-gap shall be placed in an air current of a velocity of 3 m per sec.

Care shall be taken to make all connections for the purposes of this test as short as possible.

Polyphase machines may be tested in single phase connection. The connections shall in this case be changed as often as necessary so that every phase will be subjected to the surge test.

3. Test on Turns.

2. Insulation Resistance Test.

Germany	Britain	U. S. A.
The test on turns shall be made under no-load condition by increasing the supplied and generated voltage respectively (Motors & Generators) up to the values given below. The frequency and speedrespectively may be increased correspondingly. Duration of Test: 3 Minutes Winding Rated voltage Rat	same as U.S.A. Megohms Rated volts Rated kVA or HP+1000	The insulation resistance may afford a useful indication as to whether the machine is in suitable condition for application of the dielectric test. The insulation resistance test shall be made with all circuits of equal voltage above ground connected together. Circuits or groups of circuits of different voltage above ground shall be tested separately. Test pressure if possible D. C. 500 volts. The minimum value of insulation resistance at operating temperature shall be: Megohms = voltage at terminals rating in kVA + 1000 The formula applies only to dry apparatus not for oil-immersed types. Megohms Too Too

Overloads, Starting, Commutation Test.

U. S. A. Britain Germany All machines with conti-The machines shall be Continuously rated manuous rating - must be capable of withstanding chines shall be required capable of withstanding on test the following Exto carry momentary loads cess currents or torques in of 150 per cent of the 1,5 times rated current for excess of those correamperes corresponding 2 Minutes, following cont. to the continuous rating sponding to their Brit. full load run, without delekeeping the rheostat Stand. Rating the presterious effect or resulting for rated load excitasure being maintained lasting deformation. as near the rated value tion. This test shall be carried as possible; out for Motors & Rotary Converters Motors for continuous a) Machines for contiat rated pressure; for Geneservice shall be requinuous service. rators the pressure should red to develop running Excess Ambe regulated as closely as torque at least 175% of peres: 150 per cent possible to the rated presthat corresponding to Duration: 15 seconds. sure. (See Note below.) the running torque at Motors shall be required their rated load without b) Induction Motors for to develop the following stalling. continuous service. max. running torques (or Excess torque more) without stalling. without stalmax. Torque Rating: Machines with nominal ling: 175 per cent $\binom{0}{0}$ of rated) rating. See as for Trans-(except for abnormally Continuous 16 % formers, page 32. low speed motors or Short-Time high frequencies). 20 0/0 Intermittent A. C. Motors shall be rec) D. C. shunt wound quired to develop a starting Motors or squirrel cage torque of at least $30^{\circ}/_{0}$ of induction motors for intertherated torque, when workmittent service. ing with a suitable starter Excess torque during the whole starting when runperiod in each position. ning: 200 per cent Note: Generators should Duration: 30 seconds. be amply designed so as to d) All other motors Obviously enable them to generate dutycycle rated pressure at rated for intermittent service machines must carry their peak load without speed, power factor and shall have starting torexciter voltage and at ques equal to 200 per stalling. 125% of rated current. cent of rated torque.

Overloads, Starting, Commutation Test.

> Britain: Industrial machines only. (†)							
	Motors BHP	Generators kW or kVA		ustained Overload	Momentary Overload		
Rating	per 1000 Revs. p. M.		Torque or current respectively				
Rs	not totally (%	Duration	º /o	Duration	
	below 4 to 1	below 3 to 1	25 [—]	¹/ ₂ hour [—]	50 [50]	1 Min [15 secs]	
snon	4 & upwards	3 & upwards			[3-]	[-5]	
continuous	D.C. up to 150 H.P. incl.	_	25 [—]	2 hours [—]	100 [75]	15 secs [15 secs]	
	A.C. all sizes*)				100 [75]	15 secs [15 secs]	
short t.	all sizes	all sizes	[-]	[—]	[100] 100	30 secs [30 secs]	

- †) not for motors of abnormally low speeds or high frequency.
- *) for single phase motors overloads are not yet specified.

Commutation Test.

Germany

Machines with Commutators shall work practically sparkless from no-load to full load. At overload test they must commutate in such a way so that neither commutator nor brushes are injured.

Machines with Commutators shall work practically sparkless with fixed brush setting as follows:

without	With
auxilia	ry poles
from 0,25 to 1,0 load	from no load to full load

Commutation Test.

Britain

D. C. machines shall work throughout the range from no load to the highest momentary load specified with fixed brush setting. The operation must be practically sparkless from no load to full load and without injurious sparking up to the highest momentary load specified. (

Commutation Limitation.

U.S.A.

Continuously rated machines shall be required to commutate successfully momentary loads of 150% of the Amperes corresponding to the continuous rating keeping the rheostat set for rated load excitation.

Machines for duty-cycle operation shall commutate successfully under their specified conditions. Successful operation is such that neither brushes nor commutator are injured by the test.

Efficiency *).

I) General

Germany U. S. A.

Recognized Efficiences:

- 1. Directly measured Efficiency
 Output
 - $=\frac{\text{Output}}{\text{Input}}.$
- 2. Conventional Efficiency (determined from losses).
- 1. Directly measured Efficiency
 Output
- Input

 2. Conventional Efficiency (determined from losses).

General conditions:

Unless otherwise specified the conventional efficiency is to be employed.

Efficiency figures shall correspond to normal working conditions unless stated otherwise. When using method 2 the resistances measured by D. C. shall be corrected to a reference temperature of 75°C. For measurement of other losses no temperature correction shall be made.

Unless otherwise specified the conventioal efficiency is to be employed. Efficiency figures shall correspond to rated load, sine wave form, temperature of reference (at all loads) 75°C (tests shall preferably not be made at an ambient temperature of less than 15°C). The efficiency of alternators shall be stated at the rated power factor. Sine wave shall be standard unless different wave form is inherent in the operation of the system.

^{*)} Britain: Neither Definition nor Specification regarding measurement stated. >For industrial machines the declared (actual) efficiency shall include stray load losses estimated or ascertained as closely as possible.

Efficiency.

1) General

Germany U. S. A.

Miscellaneous losses:

All losses due to auxiliary apparatus—but these only—of the machine itself shall be charged against the machine efficiency. Such are:

- a) Losses in Regulating-, Series-, Calibrating-, Shunt- and similar resistances, Choking coils, Auxiliary transformers etc. which are necessary for the regular working. (Exception see under c.)
- b) Exciter losses in case of direct or indirect coupled exciter; not in case of separate excitation.
- c) Losses in booster machines of Rotary Converters, if they form part of the converter proper but not the losses of the transformers and choking coils belonging to the converter. These losses shall be stated separately.
- d) Losses in bearings supplied with the machine but not in bearings supplied by another firm.
- e) The power consumption of the ventilating blower if this is part of the machine proper. The power consumption in case of separate ventilating blower as also that of water and oilpumps is not to be charged against the machine efficiency but shall be stated separately.

- a) Field-Rheostat Losses shall be included in the generator losses where there is a field rheostat in series with the field magnets, even when the machine is separately excited.
- b) Ventilating Blower. When a blower is supplied as part of a machine set, the power required to drive it shall be charged against the complete unit, but not against the machine alone.
- c) Other Auxiliary Apparatus such as a separate exciter for a generator or motor, shall have its losses charged against the plant of which the generator and exciter are a part and not against the generator. An exception should be noted in the case of Turbogenerator sets with direct-connected exciters, in which case the losses in the exciter shall be charged against the generator. actual energy of excitation and the field-rheostat losses, if any, shall be charged against the generator.
- d) For the Booster type of Synchronous Converters where the booster forms an integral part of the unit its losses shall be included in the total converter losses.

Section I. 22

2. Determination of Losses for Conventional Efficiency Test.

References to Explanations given below. (Britain none specified.)

		I ² R	Losses			Other Losses		
T	Stan-	no-load	load	Bearing	Brush friction			
Type of Machines	dards	Shunt windings and separately excited circuits	Arma- ture and Series windings	friction and windage	of commu- tators and collector rings	Core loss	Brush contact I ² R Loss	Stray Load Losses
D. C. Commutating	G.	1 a)	ıb)		2b, d	l)	3	4a, b)
Machines	U.S.A.	I	a)	IIa, c)	III a)	IV a)	v	
A. C. Commutating	G.	1 a)	1 a) 1 b)		2 a, 0	i)	3	_
Machines	U.S.A.	I	a)	II a)	lII a)	lV a)	v	
	G.	1 a)	1 b, c)		2 c, c	l)	3	1 e α, β)
Synchronous Motors and Generators	U.S.A.	1:	a)	II a, c)	negli- gible except when armat. revol- ving	IV b)	negli- gible except when armat. revol- ving	VI a)
Synchronous	G.	Ia)	1 a) 1 d)		2 a, d)			4 c)
Converters	U.S.A.	I a,	c)	II a)	III a)	IVa, b)	v	
Induction	G.	_	I C)	2 a)		3 if any	4 d)	
Machines	U.S.A.	Ia	, b)	IIb)	III a)	IV a, c)	V if any	VIb)
Cascade Converters	G. only.	1 a)	1 d)		2a, d)		_	4 C)

References:

Germany (G.) U.S.A.

I. I² R Losses.

- a) I2 R losses at no-load shall be calculated from resistances measured by D.C.
- b) 12 R losses due to load current shall be calculated from resistances measured by D.C.
- c) For Induction Motors the I2R losses in the secondary circuit should be calculated from the slip.

1. I² R Losses.

- a) The I2R losses shall be based upon the current and the measured resistance.
- b) The 12R loss in the Rotors of Polyphase Induction Motors should be determined from the slip whenever the latter is accurately determinable using the following aquation:

Rotor I^2R loss = $\frac{\text{output} \times \text{slip}}{}$ I - slip

Continuation: Determination of Losses for Conventional Efficiency Test.

Germany

d) For Rotary (Synchronous) Converter the I2R losses in the armature windings shall be calculated from those corresponding to its use as D. C. Generator by using the following factors:

Number of phases:	I	2	3	6	I 2
Number of sliprings:	2	4	3	6	12
Factors:	1,45	0,39	0,58	0,27	0,2

- e) Synchronous Motors and Generators. Determination of 12R plus stray load
- a) Short-circuit method: The machine with short circuited armature winding shall be driven by a calibrated auxiliary motor at rated speed and excited so that the current is equal to rated current. The input exclusive of I2R loss at no load, bearing friction and windage, brush friction and core loss is considered equivalent to I2R losses due to load plus stray load losses.
- β) Over-excitation method: The machine at no-load at rated pressure and frequency shall be overexcited so as to carry rated current. The input equivalent as under α).
- 2. Bearing friction, Brush friction windage and core losses.

Motor method: Machine shall be worked as motor at no load.

- a) A.C. machines at rated pressure. rated frequency and at no load speed.
- b) D.C. machines at rated pressure + or - the ohmic pressure drop and at rated speed.
- c) Synchronous machines with excitation regulated so as to take the minimum current.

For a) -- c):

The input minus I2 R loss and excitation losses is considered equivalent to bearing-, brush friction and windage losses as above plus core losses.

In large Slip-ring motors in which the slip cannot be directly measured by loading, the rotor I'R loss shall be determined by direct resistance measurement; the rotor full-load current to be calculated by the following equation:

Current per ring

watts output

rotor volts at standstill $\times \sqrt{3} \times K$ This applies to 3-phase motors; for 2-phase rotors use 2 instead of $\sqrt{3}$. For motors of 150 kW or larger K = 0.95. For smaller motors K decreases; no specific value stated.

c) Synchronous Converters. I2 R losses in armature windings from losses corresponding to its use as D.C. generator by using suitable factors.

II. Bearing friction and windage:

- a) General: Drive the machine from an independent motor, the output of which shall be suitably determined. The machine under test shall have its brushes removed and shall not be excited. The output represents the bearing friction and windage.
- b) Induction motors: Losses as above may be measured by running motors free at the lowest voltage at which the motors will rotate continuously at approximately rated speed; the watts input minus I2R loss, under these conditions being taken as the friction and windage.
- c) For Engine-type Generators losses as above are very small and shall be neglected.

Continuation: Determination of Losses for Conventional Efficiency Test.

Germany

d) Generator mothod: The machine shall be driven at no-load and rated speed by a calibrated auxiliary motor and excited to rated pressure. The mechanical input minus excitation losses are equivalent to losses as under c).

Note: For D. C. machines plus or minus the ohmic pressure drop.

3. Brush Contact I² R loss is calculated by assuming the pressure drop in each brush as follows:

Carbon and graphite brushes I Volt.

0,3 Volt.

Metal-graphite brushes

- 4. Stray load losses. See also $le \alpha$) and β). Stray load losses for other types are determined in accordance with the following approximate values. The per cent values correspond to output in the case of generators, to input in the case of motors, to D. C. output in the case of rotary converters. It is assumed that they vary with the square of the current.
- a) Compensated D. C. machines 0.5%
- b) Not compensated D.C. machines with or without commutating poles
- commutating poles $1^{0}/_{0}$ c) Rotary converters $0.5^{0}/_{0}$
- d) Asynchronous machines 0,5%
- e) Cascade Converters 10/0

U. S. A.

III. Brush friction of Commutator and Collector Rings.

General: Machine shall be driven as under IIa) but with brushes in contact. The brush friction is equivalent to the difference of motor output obtained in test IIa) and this test.

IV. Core loss.

- a) General: Machine shall be driven as under III but excited so as to produce at the terminals a voltage corresponding the calculated internal voltage for the load under consideration. The core loss is equivalent to the difference of motor output obtained by this test and that in test III.
- b) Synchronous Machines: The internal voltage shall be determined by correcting the terminal voltage for the resistance drop only.
- c) For Induction Motors the core loss is determined by measuring the watts input when running free at rated voltage and frequency minus no-load copper loss, bearing friction and windage.

V. Brush Contact I² R loss.

Carbon and graphite brushes I Volt Standard (pigtails attached).

Carbon and graphite brushes 1,5Volt Standard (pigtails not attached).

Metal-graphite brushes considered special.

VI. Stray load losses

- a) for Synchronous Machines s. l. l. are determined as under $1e\alpha$ (Germany) minus 1^2R losses for polyphase generators and motors. For single-phase machines stray load losses are large but not yet specified.
- b) Induction Machines with rotor removed, measure the input to the stator with different currents. Deduct I² R loss determined from resistances. The difference represents approximately the stray load losses at the different currents.

Inherent Pressure Regulation

(to be measured at the temp. attained under normal operation).

					-	,	
		2,00	Alteration of load	Regulation in %	Ger	General conditions during test	ng test
Line	Type of machine	Stan- dard	condition for purposes of test*)	of rated voltage is determined as	Speed or frequency	Excitation	Remarks
I	D. C. Generators a) shunt wound	G.	from rated load	voltage rise	rated	for a) resistance in shunt field circuit constant	brushes in nor- mal position
8	and b) separately excited	U.S.A.	to no-load	0		for b) exciting current constant	ı
8	D. C. Generators c) compound wound		from rated load to	difference between highest and lowest voltage	rated	as line 1	
4	(also series)	U.S.A.	no-load to rated load	mean value of the two results		as line I (constant resistance shunting series field)	
رح		G.		voltage variation (shall not exceed 50%) at P.F.= 0,8)			atspecified P.F.
9	Synchronous Generators	Brit.	from rated load		rated	excitation current	
7	with direct connected exciter and separate excitation	U.S.A.	to no-load	voltage rise		constant	Power Factor should be specified; if not P. F. assumed = 1
∞	Synchronous and Cascade converters	G.	from rated load	voltage rise on	rated	as line I	
6	Synchronous converters	U.S.A.	to no-load	D. C. side			
		G. U.S.A.	*) If Inherent Regulati magnetic-test Curve. Refe ") As for Germany.	*) If Inherent Regulation cannot be determined by Load Method it can be calculated from the magnetic-test Curve. Reference temperature of resistances 75° C. ") As for Germany. For Synchronous Generators I. R. can also be determined from estimated	ned by Load resistances 7 rators I. R.	ion cannot be determined by Load Method it can be calculated from the erence temperature of resistances $\gamma 5^{\circ}$ C. For Synchronous Generators I. R. can also be determined from estimated	culated from the from estimated
		Brit.	For industrial	For industrial machines: D.C. Generators as line 1. Synchr. Generators as line 6.	tors as line erators as l	e 1. ine 6.{	

Section I.

Overspeed Test.

(Britain	none	specified.)
----------	------	-------------

		Germany	U.S.A.
	Duration:	2 minutes	none specified
Line	Type of machine	Test speed Rated speed	Test speed Rated speed
I	Generators except lines 2 & 3	1,2	1,25
2	Generators driven by waterwheels	1,8	tested for max. runaway speed
3	Generators driven by steam turbines	when equipped with emergency governor acting at 10% overspeed	I,2 when equipped with emergency governor
4	Synchronous and Cascade Converters	1,2	_
5	Motors for constant speed	Test speed no-load speed 1,2	1,25
6	Motors with several rated speed	Test speed max.no-load speed I,2	Test speed max. speed (rated) 1,25
7	Motors with speed variation	1,2	1,25
8	Motors with series characteristic	Test speed max. rated speed 1,2 Test speed rated speed 1,5	not specified

Tolerances. (U.S.A. none specified.)

Guarantees for:	Tol	erances
Guarantees 101.	Germany	Britain
	Output ±0/0 of	rated
Speed of Shunt wound Motors	o to 1,1 kW 10 1,1 to 11 kW 7,5 over 11 kW 5	+50 of speed at the
Speed of Series wound Motors	o to 1,1 kW 15 1,1 to 11 kW 16 over 11 kW 7	1 713 10 or obegan me
Speed variation of D.C. Motors	10% of specifie variation	d
Speed variation of Asynchronous machine	20% of specified	slip —
Inherent Pressure Regulation of Generators	5% of rated press	ure —
Inherent Pressure Regu- lation of Rotary Converters of Cascade Converters	$\pm 1^{0}/_{0}$ of rated pre $\pm 3^{0}/_{0}$ n n	ssure —
Momentary short-circuit current of Synchronous Machines	20% of specified v	
Stationary short-circuit current of Synchronous Machines	15% of specified	ralue —
Max. running torque of Motors	100/0 of specified	ralue —
Starting torque of Motors	100/0	-
Efficiency $= \eta$	$\frac{1-\eta}{10} \text{ rounded u}$ $\frac{1}{1000}; \text{ but minimum}$	_
Power Factor $= \cos \varphi$	$\frac{1-\cos\varphi}{6} \text{ rounded}$ to $\frac{1}{1000}$; but min.	_
Temperature Rise		expressly none

Appendix to Section I.

British Electrical and Allied Manufactures Association Rules. Fourth Edition 1920.

r		2		3		
Standard pressures		Temperature Test.	f) <i>Permissible</i>			
and Frequencies.		The temp. test shall	Te	mperatu	re Rises	s.
1. Generators:		be carried out at				
1	erators:	rated output for:		Venti	lation	
D. C. 230	A. C.	ratea output for.	Insu-		_	Totally enclosed
460	550	1. Machines with con-	lation	b. ted	ally Tuck	ota clo
525	2 200	tinuous rating	Part of	unob- structed	partially obstruc- ted	T ep
	3 000 6 600	until the temperature	machine	-		į
1	11000	rise is practically con-		TRºC	TRºC	TR ºC
2. M	otors:	stant, that is until the	All			
D. C.	1 A. C.	rate of increase of	wind-			
110	100	temperature does not	ings			
220	200	exceed 10C per hour.	whose in-			
440 500	400 500		sulation			1
1	•	2. Machines with	consists			
	mers ter- als.	short-time rating	wholly			
Į		for the period defined	or in im- portant	40	47	55
	ard Highs Systems	by the rating.	part, of	(therm.)	(therm.)	(therm.)
for A		c) Methods of mea-	cotton,			
1 '	00, 6000,	'	paper, varni-			
	20000 V.	surement of Tempera-	varni- shed			
		ture of the cooling media	cloth or			
1 .	uencies:	same as B.E.S.A. rules.	similar			
50 an	nd 25.	d) Methods of mea-	ma- terials.			
Classic	fication	surement of Tempera-	terrano.	<u> </u>		L
	ating:	l ' '	Mica			
1	•	ture rises.	As-		gher va	
*	tinuous	1. Thermometer	bestos		ermissil	
b) shor	rt-time	Method (generally)	Prepa- rates	(nc	t speci	nea)
Heating.						
1		2. Resistance Method	Raw,			
1 ′	rd and max.	(for special cases).	Mica			
permissible	Tempera- ling Media:	e) Correction of Tem-	Por- celain,	,	gher va	
•	_	perature Rises for	fire		ermissil	
	25 °C (air)	Altitude.	proof	(nc	t speci	neu)
Max.	35°C (air).		Ma- terials			
b) Deterr	nination of	Temp. Rise to be	terials			
	ratures and	reduced 21/2 per cent				
Temperat	ture Rises	for each 1000 feet.			l	1
		L	<u> </u>			

Continuation: Appendix to Section I.

	4			5		6	
Insu- lation Part of machine	Ventii op-qoun TR °C	L partially S obstruc- c ted	T Totally enclosed	High Pressure Tes and Insulation R sistance. Nature of tests etc. B.E.S.A. rules! A. High Pressur Test.	as ·e	Note: E re 1. The test based on the pressure to windings migeted. H. I field winding.	the must be ne highest which the ay be sub- ce tests on generate be
Core in which wind-ings are embedded	40	47	55	Rated terminal pressure E S S S S S S S S S S S S S S S S S S	re	based on the pressure. 2. In the chines driveterwheels at to runaway	ease of ma- en by wa- nd exposed conditions
Commutator and Sliprings		55		Above 333 but not more than 1500 Volts Above	300	or otherwis to possible e sure it is rec that pressur devices sha	xcess presommended re-limiting
Alterna- tor field coils	55 (Res.)		•	1500 but not more than 2250 Volts Above 2250 Volts 2 E -	_	vided, other as under 1) B. Insu	rwise test necessary.
Shunt field coils of D.C. machines	60 (Res.)	65 (Res.)	70 (Res.)	Note: Field windings of synchronous machines intended to be started from the A. C. side are to be tested with 5000		Resistan In general ing insula tance is suf dence that ings are in to receive pressur	the follow- tion resis- ficient evi- the wind- condition the High-
Machi ditions of the air to	or othe	r cases		unless the field wind-ingsareprovided with a	-	Rated pressure	Resis- tance Megohm
of 35°C perature be reduce	rises a	s above	e) are to			Low pressure	0,25
Mica, A material	sbestos					above 350 Volts	I

Overloads, Commutation Test, Starting.

Tolerances.

a) Machines with continuous rating having limits of full-load temperature rise and unobstructed ventilation are to be capable of withstanding $25\,^0/_0$ overload for the periods:

Outputs	Duration
100 kW or HP and above	2 hours
Below 100 kW or HP not below 25 kW or HP	1 hour
Below 25 kW or HP not below 2 kW or HP	¹/2 hour
Below 2 kW or HP	5 Min.

- b) Machines as above but with partially obstructed ventilation are to be capable of withstanding $15^{\circ}/_{\circ}$ overload for the periods as above.
- c) Machines as above but of the totally enclosed class have no over-load rating except momentary as required for commutation tests.

Motors with short-time rating are to be capable of carrying:

Overload torque	Duration
100 0/0	30 Secs

Commutation test.

D. C. machines must operate throughout the range from no load to the highest specified overload with fixed brush setting. The operation must be practically sparkless from no load to full load and without injurious sparking up to the maximum specified overload.

Subject	Tolerance				
Speed of Shunt wound Motors	$\pm 5^{0}/_{0}$ of spload	peed at full temp.			
Speed of Series wound Motors	\pm 7,5% of s load	speed at full temp.			
Speed variation of Asynchron- ous machines		listed value slip			
Inherent Pressure Regulation of Generators	o,4 of spec	cified value			
	Full load Efficiency ⁰ / ₀ *)	Tolerance %:			
	≥ 95	0,5			
	< 95 to 93	0,75			
Efficiency	< 93 to 90	I			
•	< 90 to 85	1,5			
	< 85 to 75	2			
	< 75 to 65	3			
	< 65	4			
	Full load P. F. %	Tolerance 0/0:			
	≥90 2				
Power Factor	~ 90 to 05	3			
	< 85 to 75	4			
	< 75 to 65	6			
	< 65	8			
	(1/1 load Effic plus	ciency × 4) o			
Average load Guarantee for	(³ / ₄ load plus	" \times 3) sided \times 3			
Efficiency	1/2 load	" ×₂ J̄ð̄			
	1	s as above			
Observation of Temp. Rise	2	°/ ₀			
	• • • • • •	10			

^{*)} Above values apply to conventional Efficiency. For directly measured efficiency the tolerance should be increased $1/2^{\circ}/_{0}$ for Efficiencies $\geq 88^{\circ}/_{0}$ and $1^{\circ}/_{0}$ for Efficiencies $\leq 88^{\circ}/_{0}$.

SECTION II. Transformers.

Rating-Classification.

Germany	Britain	U. S. A.
a) Continuous Rating. The T. shall give its rated output for any desired period without exceeding the limits specified for observable temperature and temperature rise. b) Continuous Rating with short-time load. The T. shall give the rated output for the specified period without exceeding the limits mentioned under a). The load period is assumed to be shorter than the time required by the T. to reach the constant end temperature condition; the no-load period (secondary windings disconnected) is assumed to be of such duration to enable the T. to reach the constant no-load temperature. c) Continuous Rating. Intermittent load. Load periods of max. 5 min. are followed by no-load periods the duration of which is not sufficient to enable the T. to reach constant no-load temperature. The T. shall give the rated output with the specified relative load periods for any desired period without exceeding the limits mentioned under a)	Rating is the output at which a T. canwork con- tinuously for an unlimited period and comply with these rules.	a) Continuous Rating. The T. shall be able to operate continuously at its rated output, without exceeding any of the limitations established.

Continuation: Rating-Classification.

Britain U. S. A. Germany b) Short-Time Rating. The T. d) Short-Time Rating. b) Short-Time Rating is the output shall be able to operate at its The T. shall give the rated output during a limited rated output for the at which a T. can period to be specified in each specified period without work for a limited case without exceeding any of exceeding the limits period (to be spethe limitations established. cified in each mentioned under a). case) and comply with these rules. c) Duty-Cycle Operation. For c) Duty-cycle e) Duty-cycle Rating. purposes of rating either a con-Rating Periods under pressure tinuous or a short-time equiva-(in special cases) of max. 5 Min. are follent load may be selected which is the continuous lowed by periods during shall simulate as nearly as posrating which is which the T. is switched sible the thermal conditions of the thermal equioff (entirely), the durathe actual duty-cycle. valent of the cytion of which is not d) Nominal Rating. (For special cle of duty specisufficient to enable the cases). The nominal rating of a fied. T. to reach the tempesubstation transformer*) carrying rature of the cooling traction load shall be the KVA-The T. shall medium. output at a stated power factor give the rated load input, which, having produced under the same condia constant temperature in the tions as mentioned untransformer may be increased der c). 50 % for 2 hours, without produf) Agricultural Rating. cing temp. rises exceeding by 100 % overload is admore than 5 °C the limiting vamissible for 12 hours lues stated hereafter. These T.s per day and during should be capable of carrying approx. 500 hours per 100 0/0 overload for one minute withyear. The T. shall give out disqualifying them for conti-160% of the rated load nuous service. continously without exe) Rating of Protective Reactors. ceeding the limits men-P. R. shall be rated by: tioned under a) on 1. KVA absorbed by normal cur-100% overload as above rent. the specified limits for 2. Normal current, frequency as temperature and tempelim (delta) voltage. rature rise may be ex-3. Short circuit current which the ceeded by 100 C. P.R. is required to stand. * also for Substation machines.

Heating

Germany			Britain	U. S. A.
a) Standard- and max.	permissible	Ten	peratures of	Cooling Media.
Normal	20 º C		_	_
Max. permissible air	35°C		40 °C	40°C
Max. permissible water	25°C			250 C
Max. permissible oil	95° C		(provisionally adopted) 90 °C	90 º C

b) Determination of End-Temperatures and Temperature Rises. Heating Test.

The Heating Test shall be carried out at As one page 7. rated load with the exception of T.s with agricultural rating:

- 1. For T.s with continuous rating until the attainment of a steady Temperature. (Test started with T. warm or cold.)
- 2. For T.s with continuous rating and shorttime load. The test shall be started with the T. at constant no-load temperature and carried on for the specified period.
- 3. For T.s with short-time rating. The test shall be started with cold Transformer i. e. with the temperature of the windings within 30 C (max. higher) of the temp, of the cooling medium and carried on for the specified period.
- 4. For T.s with intermittent ratings as under c and e on pages 31 & 32. The T. shall be subjected to an intermittent load of the specified relative load periods and carried on until the attainment of a steady temperature. It shall be discontinued at the end of the last load period. For the test the duration of a load-cycle shall be 10 Minutes.

Note: For Ratings a, c and e (pag. 31 & 32) the Heating Test may be considered satisfactory if the rate of increase of temperature does not exceed 10C per hour and if the temp. is 50 C below the guaranteed value.

5. For T.s with agricultural rating. For the purposes of Heating Test the 60% overload is considered as rated load. The 100% overload heating test is started with the Transformer on constant rated load temperature and continued until the attainment of a steady temperature but not longer than 12 hours.

Air blast Transformers Correction of observed Temp. Rise:

The Temp.

Rise as stated

on page 36 &

37 shall be reduced by 1 per cent for each 20C that the temperature of the air entering the Transformer

is below 40°C.

As on page 7.

Further:

Air-blast Transformers. Correction of observed temp. rise due to difference in resistance when temp. of ingoing air t differs from that of the standard of reference i. e.

> 274,5 234,5 + t

400 Cels.

Loading of T.s for Temperature Test.

The conditions shall be such to give losses as nearly as possible equal to those obtained under normal or specified load conditions.

air kW.

dium kW.

 W_K = heat carried off by other me-

Continuation: Heating.

Britain U.S.A. Germany c) Methods of measurement of Temperature of the cooling media. The value to be adop-For 1. Transformer with air-cooling The air temperature ted for the ambient temp. (self-cooling). For 2. Transformer oil-immersed, during a test, is the mean shall be taken as the mean of the readings of the self-cooling. For 3. Transformer oil-immersed of the readthermometers taken at ings of the equal intervals during with separate oil cooler (air cooled) the last quarter of the thermometers and forced oil circulation. taken at equal duration of test. The temp, of the cooling medium intervals duris to be taken as the mean of the ing the last ambient air temperatures during the quarter of the last quarter of the test period. duration οf For 4. T.s of air blast type. the Test. For For 5. T.s oil-immersed, tank forced pipeventilaair cooled. tion or forced-For 6. T.s oil-immersed, tank forced draught, the air cooled also forced oil circulation. air temp. is to For 7. T.s oil-immersed with sepabe measured rate oil cooler which itself is forced by a thermoair cooled and forced oil circulation. meter placed The temp. of the cooling medium in the current is to be taken as the mean of the of the intemperatures of the air at the air coming air. inlet taken during the last quarter of the test period. Water-cooled T.s. The For water cooled types: temp. rise shall be based 8. With individual parts only cooled. entirely upon the temp. Windings not immersed. of the cooling water. If 9. Oil-immersed, cooler inside of tank. under assumed standard 10. Oil-immersed, cooler outside of conditions (water 25°, air 40°C) the amount tank and forced oil circulation. The temp. of the cooling medium of heat carried off by shall be taken as the mean of the the air is $15^{0}/_{0}$ or more of the total, the temp. temperatures of the water at the water inlet taken during the last quarter of the cooling water of the test period. during test should be If the amount of heat carried off maintained within 50 C by the ambient air is considerable, of that of the surroundthe temp, of the cooling medium is ing air. Where this to be considered the mean value impracticable the derived from the formula ambient temperature $T_M = \frac{T_K W_K + T_L W_L}{W_K + W_L}$ should be determined from the change in the resistance of the wind- $T_M = \text{mean value of temp. of cooling}$ ings, using a disconnecmedium. ted Transformer, $T_L = \text{temp. of ambient air.}$ supplied with the normal $T_{\mathbf{K}} = \text{temp. of other cooling medium.}$ amount of cooling water W_L = heat carried off by ambient

until the temp. of the

windings has become

constant.

Continuation: Heating.

Germany	Britain	U.S.A.
d) Methods of measu	rement of Ter	nperature rises.
The temperature rise of windings of air cooled t.s is defined as the higher of the two values as below 1. Mean temperature rise by Resistance Method. 2. Temperature rise of the hottest accessible spot measured by Thermometer. For oil immersed T.s Method I only shall be used. For T.s for very heavy currents the Resistance method is not exact; special arrangements for measuring oil temperature only are recommended.	Resistance Method for windings	The temperature of the windings shall be measured by their increase of resistance and by thermometers whichever measurement yields the higher temp., that temp. shall be taken as the highest observable temperature by method 2 (page 10).
Temp. rise of core shall be determined by Thermometer Method at the hottest accessible spot.	Temp. rise of core same as Germany.	Temp. rise of core same as Germany.
Temp. rise of oil shall be determined by Thermometer measured near oil surface in the tank.	Temp. rise of oil shall be determi- ned by thermometer in oil.	Temp. rise of oil same as Germany.
e) Correction of Te	mperature Ris	e for Altitude.
As on page 11.	As on page 11.	As on page 11 but water-cooled T.s are exempt.

f) Permissible Temperature Rises. (ET = End Temperature; TR = Temp. Rise.)

		TR*) °C	40			55		55	1	so 55 sased or vater of 25°C	
		ET o	80			95		95	ı	80 55 based or water of 25°C	
	U.S.A.	Class of Insulation	Class O		Class A	same as Germany Items 2 & 3		Class A		Class A	And the second s
J		Type of Transformer	Air cooled or air blast	Air cooled or air blast Oil cooled					Water		
5		TR °C*)	45	2	55	55	75	55			
		ET °C	8	7	95	95	115	95*)			
1 — Fild rempelment)	Britain	Insulation	not impregnated	or oil- immersed	impregnated Class A	Class A	Class B	insulating materials immersed in oil			
vises.		Ins	cotton,	silk, paper and	similar material	enamelled wire	Asbestos Mica etc.				
וחוב	Germany	Type	Air cooled			лiА		Oil cooled			
npera		TR °C	50	50		9		70	80	5°C more than Items 1—5	
10 10 10		ET 0C	85			70	S	105	115	5°C than	
I) rermissio		ss of Insulation	not impregnated	not impregnated but coil dipped in		impregnated or compounded i. e. impregnating material fills the space between conductor and insulation and between the fibres		immersed in oil	nd Asbestos preparates	Raw Mica, Porcelain or other fire-proof materials	
		Class		·	Fibrous material	as paper, cotton, silk,	8 000 8		Mica- and As	Raw Mi	
		məal	-		8		n	4	<u>بر</u>	9	

I	Part of Transformer	ner not	5°C more	nore							
5	insulated		than Items I—5	tems 5							
ပိ	Continuously short circuited	rcuited	as other windings	her ngs					·		
	windings		by resist. method	sist.					Part of Transformer	ansformer	ET TR
	air cooled types (windings not immersed)	types mmersed)	95	99	cores		restr by i	restricted by influ-	300	air cooled type	restricted by influ-
S	core in oil-immersed types	1	105	70	Iron		enc adja parts	ence on adjacent parts only		oil cooled type	adjacent parts only
	Oil near surface	a)	95	99		oil	8	50	iio	=	
	All other parts		restricted by influ- ence on adjacent parts only	cted flu- on cent only					All other parts	r parts	restricted by influ- ence on adjacent parts only
₹ .	*) Method of measurement: Items 1—6. Resistance M ", 7-12. Thermometer	surement: Resistance Method. Thermometer "	10d.		*	*) Method of measurement: see page 35.	:		*) Method of me see page 35.	*) Method of measurement: see page 35.	nt:
ote istal sed coo coo	Note: The end temperature must under no circumstances be exceeded. The temp. rise may be exceeded only in such cases where the temp. of the cooling medium is always so low that the end temperatures (as above) will not be reached.	re must un he temp. r s where th s so low th	der no ise ma ne tem nat the reache	cir- y be p. of end							

I. High-Pressure Tests.

	Germany			Britain			U.S.A.	
Nature of Tests	1. High-Pressure Test 2. Surge Test for T.s f 1000 to 60000 Vol 3. Test on Turns	High-Pressure Test Surge Test for T.s from 1000 to 60000 Volts Test on Turns	1. Higl 2. Insu	1. High-Pressure Test 2. Insulation Resistance Test	it ace Test	i. Test	 Test of Dielectric Strength Insulation Resistance Test 	Strength ce Test
I.	1. High-Pressure Test	Test	I	1. High-Pressure Test	Test	1. Test	1. Test of Dielectric Strength	Strength
Wave form.	snuis	sinusoidal		sinusoidal			sinusoidal	
Frequency	rated, or	rated, or 50 cycles	rated in	general any between 25 and 100	oetween 25 o	not 60 cy	not less than rated 60 cycles recommended	ted inded
Duration	one 1	one minute		one minute			one minute	
Temperature during Test	working T	Temperature	WOL	working Temperature	ture	worl	working Temperature	ture
Type	Rated	Test pressure	Tvne	Rated	Test pressure	Type	Rated output Normal	Test pressure
Transformer	pressure E	Volts min.		Output	Volts	Transformer	circuit voltage E	Volts
	up to 10000 Volts	3,25 E 2500		below 746 Watts	2 E + 500		for 25 Volts or lower	500
A II	over 10000 Volts	1,75 E+ 15 000	All	746 Watts and above	2 E + 1000	Household devices	notover 660 Watts n n 275 Volts	\$00
Air cooled	up to	if measured cold: 3,74 E 2800	Transf.	below 746 Watts	1,5 E + 375	Standard	all	2 E + 1000
(windings not immersed)	over 10 000 Volts	if measured cold: 2,02 E + 17250	in service (not new)	746 Watts and over	1,5 E + 750	Distributing Transformers	from 55° to 45°° Volts	primary: 10000 secondary: 2 E + 1000

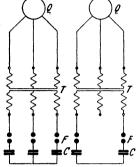
: 2,73 E/	+ 1000 E' voltage of circuit	o ground	same as apparatus to which connected	al voltage of machine is
	over 300 Volts		l	Note: E represents the normal voltage circuit to which the machine nected.
A. C. single	permanently grounded (not 3-phase	with earthed neutral)	Auto Trans- former	Note: E represente connected.
\$000	10000	2 E + 1000	same as apparatus to which connected	Note: The test must be based on the highest pressure E to which the windings may be subjected. T.s are to have the same test between high pressure winding and core as between high pressure winding and low pressure winding.
primary less than 2000 Volts	primary 2000 Volts and above	secondary (L. P.) windings		Note: The test must be based on the highest pressure E to which the windings may be subjected. T.s are to have the same test between high pressure winding and core as between high pressure winding and low pressure winding.
Transf.	for direct connection to	circuit	Auto Trans- former	Note: 1. The test mus pressure E to be subjected. 2. T.s are to ha high pressure between high low pressure.
8 E + 2000	ci	- + - 7 500000		nal pressure when testwindings against core. d regulating T.s with y and secondary windterminal pressure of hich the windings are ries. cted windings, the sum pressures. T.S with variation of use by switching officional windings, the al voltage necessary ary voltage. I. it times rated terant voltage the current continuously nor must uctuations.
up to		3000 Volts 20		
	Transformer Bushings			E represents: 1. The rated terminal ing individual wind re separate primary at ings, the rated teather connected in series. 3. For series connected to the terminal preduction of the terminal preduction of the terminal preduction of the terminal preduction of the terminal preduction primary terminal for max. secondary 5. For T.s with one nently grounded 1, minal pressure. Note: At constant must not increase contents.

Transformers Section II.

2. Surge Test (Germany only).

The surge test (Purpose see under Section I) shall be made on the factory test bed with the completely assembled transformer with windings for rated voltages from 25 to 60 kV in accordance with the diagrams of

connections as shown below.



The Transformer winding on test shall be connected to cables or condensers (C) over sphere sparkgaps (F) with solid spheres of at least 50 mm diameter. — The test capacitance of the cables or condensers shall be as follows:

Rated Voltage E kV	Capacitance C of each phase min. μ F. (Mikrofarads)	Suitable form of capaci- tance
2,5 up to 6	0,05	cable or condenser
,, ,, 15	0,02	,, ,, ,,
,, ,, 35	0,01	" " "
,, ,, 60	0,005	condenser

Details of test as for machines Section I.

3. Test on Turns.

2. Insulation Resistance.

2. Insulation Resistance Test.

Geri	nany	Britain	U. S. A.
under no-load creasing of the up to the valu The frequency correspondingly	eest shall be made condition by in- supplied voltage es given below. can be increased est: 5 Minutes.	same as U.SA.	The insulation test may afford a useful indication as to whether a machine is in suitable condition for application of the dielectric test. The insulation test shall be made with all circuits of equal voltage above ground connected together. Circuits or groups of circuits of
Output kVA	Test voltage		different voltage above ground shall be tested separately.
	Rated voltage		Test pressure if possible D.C. 500 Volts.
up to 1000	2		Minimum values in Megohms
over 1000	If possible 2; min. 1,3		for dry apparatus (not oil-immersed) see page 17.

Working in parallel (Germany only).

It is recommended that T.s of different outputs and with a ratio of outputs over 1:3 shall not be required to work in parallel continuously.

T.s shall be considered to work in parallel satisfactorily if the rated impedance voltages do not differ from their mean value by more than $\pm 10^{0}/_{0}$. T.s with tappings shall not in every case be required to work in parallel satisfactorily on all ratios.

Overloads.

In general none specified with the exception of agricultural T.s see page 32.

none specified In general none specified with the exception of nominal rating see page 32.

Efficiency, Transformer Losses.

Germany U. S. A.

1. General.

Recognized Efficiencies: Losses only mentioned, therefore Conventional Efficiency implicitly recognized only.

Miscellaneous losses: The power consumption of motors for separate ventilating blowers as also that of water-or oil-circulating pumps shall be stated separately.

General conditions: see page 20.

Recognized Efficiencies:

1. Directly measured Efficiency

 $=\frac{\text{Output}}{\text{Input}}$

2. Conventional Efficiency (determined from losses).

General conditions: see page 20.

2. Classification of Losses and their Measurement.

No-load Losses are considered equivalent to the input at normal rated pressure on the primary side, at rated frequency and with the secondary terminals disconnected. They include the core loss, the dielectric loss and the I²R loss due to the no-load current. The n. l. l. are generally measured from secondary side.

Load Losses are considered equivalent to the I²R losses at rated current and frequency, at working temperature measured within the terminals.

They shall be measured by applying the impedance voltage to the T. with the secondary windings short circuited. Stray-load losses due to eddy-currents are included in the losses measured as before.

No-load Losses include the core loss, the I²R loss due to the exciting current and the dielectric loss in the insulation.

They shall be measured with open secondary circuit at the rated frequency, and with an applied primary voltage giving the rated secondary voltage plus the IR drop which occurs in the secondary under rated load conditions.

Load Losses include I²R losses and stray load-losses due to eddy-currents caused by fluxes varying with the load.

They shall be measured by applying a primary voltage, at rated frequency, sufficient to produce rated load current in the with the windings secondary windings short-circuited.

Inherent Regulation

to be measured at the temperature attained under normal operation.

The I. R. of a T. at a specified Power Factor is the rise of the secondary voltage in per cent of the rated secondary pressure if the load is altered from rated load to no load and with primary voltage and frequency constant.

Britain	U.S.A.
Sar —	ne as Germany. Unless a P. F. is specified the regulation is understood to refer to P. F. = 1.

Tolerances.

Germany	for losses	100/0 of copper and core losses.
Britain	for temp, rise	expressly none.

Appendix to Section II (Transformers).

British Electrical and Allied Manufacturers Association Rules. Fourth Edition 1920.

Rating Classification.

- a) continuous.
- b) short-time.

Heating.

- a) Standard- and max. permissible temp. of cooling media.
- b) Determination of End-Temp. and Temp. Rises.
- c) Methods of measurement of temperatures of cooling media.
- d) Methods of measurement of Temperature Rises:

oil cooled types: Resistance Method, air " " : Thermometer "
Temp. Rise of oil measured by thermometer as also core temperature.

- e) Correction for Altitude same as Appendix to Section I.
- f) Permissible Temp. Rises.

Class of Insulation	Type of Trans- former	ET °C	TR*)
Fibrous material as paper, cotton, silk	1	85	50
	oil cooled	85	50
Mica and Asbestos preparates		Higher values permissible (not specified)	
Raw Mica or other fire-proof material			

*) Method of measurement see under d).

Note: Transformers for tropical conditions or other cases where the air temp. is in excess of 35°C the permissible temp. rise (as above) is to be reduced by 20°/0 except for Mica or Asbestos Insulation.

High Pressure Test and Insulation Resistance.

Nature of Tests etc.: same as B.E.S.A.

1. High Pressure Test.

Rated terminal	Test pressure			
pressure E	Volts	min. Volts		
not more than 333 Volts	1000			
above 333 Volts not more than 500 Volts	3 E	1500		
Above 1500 Volts but not more than 2250 Volts	4500	_		
above 2250 Volts	2 E			

Note: same as B. E. S. A. page 38 & 39.

2. Insulation Resistance. In general the following insulation resistance is sufficient evidence that the windings are in condition to receive the high-pressure test.

Rated pressure	Resistance megohms	
low pressure	0,25	
above 350 Volts	I	

Overloads.

Overload capacity:

 $25^{0}/_{0}$ for 2 hours, $100^{0}/_{0}$ for 30 secs.

Tolerances.

Full-load Efficiency (by summation of losses)	Toleranc e	
98 °/0 or higher	0,25 0/0	
below 98 º/o	0,4 %	
average load	see page 30	

- Erläuterungen zu den Vorschriften für die Konstruktion und Prüfung von Installationsmaterial, den Vorschriften für die Konstruktion und Prüfung von Schaltapparaten für Spannungen bis einschl. 750 V und den Normalien über die Abstufung von Stromstärken und über Anschlußbolzen. Im Auftrage des Verbandes Deutscher Elektrotechniker herausgegeben von Georg Dettmar, Generalsekretär des Verbandes. Mit 46 Textabbildungen. Unveränderter Neudruck. 1922.

 GZ. 3,6; 3,60 Fr.; 0,75 \$; 3 sh.
- Erläuterungen zu den Normalien für Bewertung und Prüfung von elektrischen Maschinen und Transformatoren, den normalen Bedingungen für den Anschluß von Motoren an öffentliche Elektrizitätswerke und den Normalien für die Bezeichnung von Klemmen bei Maschinen, Anlassern, Regulatoren und Transformatoren. Im Auftrage des Verbandes deutscher Elektrotechniker herausgegeben von Georg Dettmar. Sechste Auflage.
- Erläuterungen zu den Vorschriften für die Errichtung und den Betrieb elektrischer Starkstromanlagen einschließlich Bergwerksvorschriften und zu den Merkblättern für Starkstromanlagen in der Landwirtschaft. Im Auftrage des Verbandes Deutscher Elektrotechniker herausgegeben von Geh. Reg.-Rat Dr. C. L. Weber. Dreizehnte, vermehrte und verbesserte Auflage. 1923.

 GZ. 3.3; 4 Fr.; 0,80 \$; 3 sh. 4 p.
- Arnold-la Cour, Die Wechselstromtechnik. Herausgegeben von Professor Dr.-Ing. E. Arnold, Karlsruhe. In fünf Bänden. Unveränderter Neudruck. Erscheint im Frühjahr 1923.
 - I. Theorie der Wechselströme. Von J. L. 1a Cour und O. S. Bragstad. Zweite, vollständig umgearbeitete Auflage. Mit 591 Textfiguren.
 - II. Die Transformatoren. Ihre Theorie, Konstruktion, Berechnung und Arbeitsweise. Von E. Arnold und J. L. 1a Cour. Zweite, vollständig umgearbeitete Auflage. Mit 443 Textfiguren und 6 Tafeln.
 - III. Die Wicklungen der Wechselstrommaschinen. Von E. Arnold. Zweite, vollständig umgearbeitete Auflage. Mit 463 Textfiguren und 5 Tafeln.
 - IV. Die synchronen Wechselstrommaschinen. Generatoren. Motoren und Umformer. Ihre Theorie, Konstruktion, Berechnung und Arbeitsweise. Von E. Arnold und J. L. la Cour. Zweite, vollständig umgearbeitete Auflage. Mit 530 Textfiguren und 18 Tafeln.
 - V. Die asynchronen Wechselstrommaschinen.

 1. Teil: Die Induktionsmaschinen. Ihre Theorie, Berechnung, Konstruktion und Arbeitsweise. Von E. Arnold und J. L. la Cour unter Mitarbeit von A. Fraenckel. Mit 307 Textfiguren und 10 Tafeln.

 2. Teil: Die Wechselstromkommutatormaschinen. Ihre Theorie, Berechnung, Konstruktion und Arbeitsweise. Von E. Arnold,
 - Theorie, Berechnung, Konstruktion und Arbeitsweise. Von E. Arnold, J. L. la Cour und A. Fraenckel. Mit 400 Textfiguren, 8 Tafeln und dem Bildnis E. Arnolds.

- Theorie der Wechselströme. Von Dr.-Ing. Alfred Fraenckel. Zweite, erweiterte und verbesserte Auflage. Mit 237 Textfiguren. 1921. Gebunden GZ. 11; gebunden 11,35 Fr.; gebunden 2,30 \$; gebunden 9 sh. 6 p.
- Ankerwicklungen für Gleich- und Wechselstrommaschinen. Ein Lehrbuch. Von Prof. Rudolf Richter, Karlsruhe. Mit 377 Textabbildungen. Berichtigter Neudruck. 1922. Gebunden GZ. 11; gebunden 14 Fr.; gebunden 2,80 \$; gebunden 11 sh. 9 p.
- Kurzes Lehrbuch der Elektrotechnik. Von Dr. Adolf Thomälen, a. o. Professor an der Technischen Hochschule Karlsruhe. Neunte, verbesserte Auflage. Mit 555 Textbildern. 1922. Gebunden GZ. 9; gebunden 9,60 Fr.; gebunden 1,95 \$; gebunden 8 sh.
- Die wissenschaftlichen Grundlagen der Elektrotechnik. Von Prof. Dr. Gustav Benischke. Sechste, vermehrte Auflage. Mit 633 Abbildungen im Text. 1922. Gebunden GZ. 15; gebunden 18 Fr.; gebunden 3,60 \$; gebunden 15 sh.
- Hilfsbuch für die Elektrotechnik. Unter Mitwirkung namhafter Fachgenossen bearbeitet und herausgegeben von Prof. Dr. Karl Strecker, Geh. Oberpostrat. Zehnte, umgearbeitete Auflage. In drei Teilen.

 In Vorbereitung.
- Elektrische Starkstromanlagen. Maschinen, Apparate, Schaltungen, Betrieb. Kurzgefaßtes Hilfsbuch für Ingenieure und Techniker sowie zum Gebrauch an technischen Lehranstalten. Von Studienrat Dipl.-Ing. Emil Kosack, Magdeburg. Sechste, durchgesehene und ergänzte Auflage. Mit 296 Textfiguren. 1923. GZ. 5; gebunden GZ. 5,8; 6,25 Fr.; gebunden 7,25 Fr.; 1,25 \$; gebunden 1,45 \$; 5 sh. 3 p; gebunden 6 sh.
- Schaltungen von Gleich- und Wechselstromanlagen. Dynamomaschinen, Motoren und Transformatoren, Lichtanlagen, Kraftwerke und Umformerstationen. Ein Lehr- und Hilfsbuch. Von Dipl.-Ing. Emil Kosack, Studienrat an den Staatl. Vereinigten Maschinenbauschulen zu Magdeburg. Mit 226 Textabbildungen. 1922. GZ. 4; gebunden GZ. 6; 6,80 Fr.; gebunden 10 Fr.; 1.75 \$; gebunden 2 \$; 5 sh. 8 p; gebunden 8 sh. 3 p.
- Der Drehstrommotor. Ein Handbuch für Studium und Praxis. Von Prof. Julius Heubach, Direktor der Elektromotorenwerke Heidenau G. m. b. H. Zweite, verbesserte Auflage. Mit 222 Abbildungen. 1923. Gebunden GZ. 14,5; gebunden 18 Fr.; gebunden 3.60 \\$; gebunden 15 sh.
- Elektrotechnische Meßinstrumente. Ein Leitfaden. Von Konrad Gruhn, Oberingenieur und Gewerbestudienrat. Zweite, vermehrte und verbesserte Auflage. Mit 321 Textabbildungen. 1923. Gebunden GZ. 5,8; gebunden 6,40 Fr.; gebunden 1.30 \$; gebunden 5 sh. 6 p.

Die Grundzahlen (GZ) entsprechen den ungefähren Vorkriegspreisen und ergeben mit dem jeweiligen Entwertungsfaktor (Umrechnungsschlüssel) vervielfacht den Verkaufspreis. Über den zur Zeit geltenden Umrechnungsschlüssel geben alle Buchhandlungen sowie der Verlag bereitwilligst Auskunft.